学术期刊可以用微信做什么，快来看看！

微信自动应答服务平台
微时代 微革命

微服务
移动互联网时代的营销革命
简单快捷 • 高效互动 • 随时随地 • 广泛传播

微信扫一扫 开启智慧“微服务”
Compound parabolic concentrator applied as receiving antenna in scattering optical communication

Jingyue Fang (方靖岳)¹, Hailiang Zhang (张海良)², Honghui Jia (贾红辉)², Hongwei Yin (尹红伟)², Shengli Chang (常胜利)², and Shiqiao Qin (秦石乔)²

¹College of Optoelectronic Science and Technology, National University of Defense Technology, Changsha 410073, China
²College of Science, National University of Defense Technology, Changsha 410073, China
*E-mail: fjy_nudt@yahoo.com.cn
Received August 10, 2009

The two-dimensional (2D) compound parabolic concentrator’s (CPC) characteristics are analyzed. It is shown that CPC’s height is taller and its light collecting ability is stronger with the CPC’s field of view decreasing when the bottom radius is unchanged. According to the ZEMAX analysis, CPC is good at collecting optical signal, and the antenna combining CPC with hemispherical lens can gather more optical signal than a single CPC or CPCs combined in series. The light propagation of scattering optical communication based on multiple scattering is simulated by Monte Carlo method, and the results show that using CPC as receiving antenna can strengthen communication system’s signal collecting ability and increase its communication distance.

Gain is an important parameter which reflects CPC’s light-gathering ability. According to the maximum gain condition[7]: \( \frac{dx}{dy} = 0 \), we obtain

\[ a_{\text{max}}(\theta_0) = x_{\text{max}} = b / \sin \theta_0, \]  \hfill (2)

where \( a_{\text{max}} \) is the maximum of CPC’s receiving aperture radius and \( h_{\text{max}} \) is the maximum of CPC’s height. According to the definition of the gain, we obtain the maximum two-dimensional (2D) gain as

\[ c_{\text{max}}(\theta_0) = a_{\text{max}}(\theta_0) / b = 1 / \sin \theta_0. \]  \hfill (4)

In free-space ultraviolet (UV) communications, the UV source transmits information through atmospheric scattering. The receiver side usually adopts a receiving antenna to strengthen the signal collecting ability to increase the system’s communication distance because of the strong effect of atmospheric attenuation on optical signal[1−5]. Usually, we use paraboloid antenna as the receiving antenna. Compound parabolic concentrator (CPC) is a non-imaging concentrator based on marginal optical principle. It is used as a radiation detector in high-energy physics. Because all of the rays in the range of receiving angles could be connected to the detector, it was widely used for concentrating solar radiation in the 70s of the last century. In this letter, we analyze the CPC’s structure and its optical characteristics. We propose to use the CPC in scattering optical communication as a receiving antenna since it can gather feeble signals and increase communication distance.

The CPC’s focus is set in different positions when it is combined with different detectors. There are four kinds in usual: flat, upright, triangle, and tube[6]. In this letter, the structures and traits of flat CPC are discussed.

The generatrix of CPC is composed of a section of parabola and a straight (see Fig. 1). The CPC’s profile curve equation is

\[ (x \cos \theta_0 + y \sin \theta_0)^2 + 2b(1 + \sin \theta_0)^2 x - 2b \cos \theta_0 (2 + \sin \theta_0) y - b^2(1 + \sin \theta_0)(3 + \sin \theta_0) = 0, \]  \hfill (1)

where \( \theta_0 \) is the nip angle of axis [FP] and CPC’s symmetrical axis \( oy \), and \( b \) is CPC’s bottom radius. According to Eq. (1), we know that flat CPC’s structure is determined only by \( \theta_0 \) and \( b \).

Gain is an important parameter which reflects CPC’s light-gathering ability. According to the maximum gain condition[7]: \( \frac{dx}{dy} = 0 \), we obtain

\[ h_{\text{max}}(\theta_0) = y_{\text{max}} = b(1 + \csc \theta_0) / \tan \theta_0, \]  \hfill (3)

Assuming that CPC’s bottom radius \( b \) is 1 cm, when \( \theta_0 \) is 5°, \( c \) approximates 11.47 and \( h \) approximates 143 cm; when \( \theta_0 \) is 15°, \( c \) approximates 3.86 and \( h \) approximates 18 cm; when \( \theta_0 \) is 30°, \( c \) approximates 2 and \( h \) approximates 5 cm. The CPC has a high gain and it will be higher as \( \theta_0 \) is smaller. Figure 2 shows the three-dimensional (3D) CPCs with different \( \theta_0 \) values. The receiving aperture radius, height, and gain of CPC vary indirectly with the change of \( \theta_0 \).

Figure 3 shows the ray-tracing results of CPC’s cross section. Rays whose incident angles are in the range of \( \{ \theta | -\theta_0 < \theta < \theta_0 \} \) are reflected and arrive at the CPC’s bottom. According to the results of ray-tracing, rays whose incident angles are within the receiving range would be reflected to the bottom and the gain is \( c_{\text{max}} \). So, the angle \( \theta_0 \) is CPC’s field of view.

Intercept ratio is defined as \( k = h / h_{\text{max}} \) (\( h \leq h_{\text{max}} \)).
Then Eq. (4) is equivalently written as
\[
c(\theta_0, k) = \left\{ - (1 + \sin \theta_0)[\sin \theta_0 + k(1 - \sin \theta_0)] \\
+ 2\sqrt{k \cos^2 \theta_0 + \sin^2 \theta_0} \right\} / [(1 - \sin \theta_0) \sin \theta_0]. \tag{5}
\]
It is clear that \(c\) is related to \(k\) by observing Eq. (5). In detail, \(c\) directly varies as \(k\) changes, and the faster \(c\) increases, the larger the value of \(k\) is; if the value of \(\theta_0\) is relatively small, \(c\) is influenced significantly by \(k\); when the value of \(\theta_0\) is larger, \(k\) affects \(c\) slightly (see Fig. 4).

On the assumption that CPC\(_1\) and CPC\(_2\) have the same bottom radius and their fields of view are \(\theta_1, \theta_2\) (\(\theta_1 > \theta_2\)), we get \(h_{max}(\theta_1) < h_{max}(\theta_2)\) and \(c_{max}(\theta_1) < c_{max}(\theta_2)\). We assume that
\[
c(\theta_2, k_2) = c_{max}(\theta_1, 1), \tag{6}
\]
and then we get
\[
k_2 = \left\{ 2 - \sin \theta_2[1 + \sin \theta_2 + (1 - \sin \theta_2)/\sin \theta_1] \\
- 2\sqrt{(1 - \sin \theta_2)(1 - \sin \theta_2/\sin \theta_1)} / \cos^2 \theta_2 \right\}. \tag{7}
\]
Figure 5 shows CPC\(_2\)'s intercept ratio curve under the conditions that CPC\(_1\) and CPC\(_2\) have the same gain and bottom radius when the CPC\(_1\)'s fields of view are 40°, 50°, and 60°, respectively. It is indicated that when CPC\(_1\) and CPC\(_2\) have the same height, CPC\(_2\)'s light-gathering ability is stronger; when CPC\(_1\) and CPC\(_2\) have the same gain, CPC\(_2\)'s height is lower.

We can draw a conclusion that CPC owns large field of view and strong light-gathering ability. Thus we can design a needed CPC with given \(b\) and \(\theta_0\). When the bottom radius is given, the height and gain increase as the field of view decreases. We should choose the value of \(k\) (usually 0.5–0.8) properly, and then we can reduce the CPC’s height to advance the machining and employment without influencing the light-gathering ability markedly.

We simulated the 3D-CPC’s light collecting ability by using ZEMAX when we chose a circular diffuse cosine source to simulate the distribution of optical signal after the atmospheric scattering. The source’s rays emit in a cosine distribution of the form
\[
I(\theta) = I_0 (\cos \theta)^{C_n}.
\]
The larger \(C_n\) is, the narrower the distribution becomes. On the assumption that we set the parameters of the source like Table 1, and ignore the energy loss resulting

<table>
<thead>
<tr>
<th>Analysis</th>
<th>Power (W)</th>
<th>Cosine Exponent Width(cm)</th>
<th>Width(cm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rays</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>10(^5)</td>
<td>1</td>
<td>2</td>
<td>4</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Table 2. Detector’s Incoherent Irradiance</th>
</tr>
</thead>
<tbody>
<tr>
<td>Size (cm)</td>
</tr>
<tr>
<td>-----------</td>
</tr>
<tr>
<td>Fig. 6</td>
</tr>
<tr>
<td>Fig. 7(a)</td>
</tr>
<tr>
<td>Fig. 7(b)</td>
</tr>
<tr>
<td>Fig. 7(c)</td>
</tr>
<tr>
<td>Fig. 7(d)</td>
</tr>
</tbody>
</table>
from the CPC’s reflection and the hemispherical lens’ absorption, we obtain the results shown in Table 2, Figs. 6 and 7 which are calculated by ZEMAX’s Monte Carlo ray-tracing method.

Figure 6 shows the detector image of the incoherent irradiance without antenna. Figure 7 shows the detector image of the incoherent irradiance using different CPCs as its antennas. Total powers in Table 2 show that using CPC as an antenna could be good for collecting the optical signal. The antenna combining CPC with hemispherical lens can gather optical signal more efficiently than a single CPC, which is equivalent to augmenting the antenna’s receiving caliber when the size of detector is fixed (see Figs. 7(a) and (b))[8]. But the hemispherical lens should be designed appropriately, since it is difficult to machine and its larger size will lead to more absorption loss of energy. Figures 7(c) and (d) show that it could not strengthen the light collecting ability by combining CPCs in series. Though the antenna’s receiving caliber is bigger, part of the incident rays of the front CPC cannot arrive at the bottom of the latter one when the detectors’ sizes are the same.

Scattering optical communication uses atmospheric scattering as its channel and optical signals will attenuate acutely by scattering and absorption of atmosphere which limits the communication system’s corresponding range. Simultaneously, optical signals will distribute in the whole sky by the scattering. So we need a reflection antenna with large field of view and high gain, and CPC satisfies these requirements.

We simulated the propagation of optical signals with Monte Carlo method[9-11]. We got the received signals’ statistical information of flying time and detectable weight by tracing the generation, collision, and disappearance of large mount of photos (about 108).

On the assumption that CPC’s field of view is 20° and its bottom radius is 1 cm, we simulated the propagation under a given condition (the detecting distance is 500 m and the stadia is 23 km) by Monte Carlo method. If the emission energy of optical pulse is 1 J, the signals’ energy arriving at the detector will be about 3.25 nJ using no antennas and 11.20 nJ using CPC as the receiving antenna, respectively. Figure 8 shows the results in the form of pulse response curves from which we know that using CPC can strengthen the system’s signal-gathering ability.

We manufactured a CPC by numerical control machine. Then we deposited an aluminum film on the CPC’s inner surface by thermal evaporation coating. Its receiving angle was 30° and bottom radius was 3 cm. To validate the CPC antenna’s validity, we used low-pressure mercury lamp as light source and set the communication distance as 40 m. What’s more, an obstacle (height: 1.5 m, width: 1 m, thickness: 0.5 m) kept out the direct light from the source to the receiver which was mainly composed of CPC, filter, and photomultiplier tube (PMT).

Table 3 shows the receiver’s outputs with and without using CPC as antenna at different receiving angles. The CPC antenna’s gain is about 1.8, which is far from the theoretical value 4. The reasons are given below. 1) Because the process level is relatively low and the surface roughness of CPC is not ideal, rays cannot propagate ideally to the focal plane (CPC’s bottom). 2) The degree of vacuum is not high and the CPC’s surface is not clean enough during the coating process, which causes the density of CPC’s films being not high. So the light might not propagate ideally to the focal plane. 3) The CPC’s bottom radius is 3 cm and the filter’s radius is 1 cm, so the CPC cannot tightly combine with the filter subsequently connecting with PMT. So a part of light energy dissipates.

![Fig. 6. Detector image of the incoherent irradiance with no antenna. The distance between source and detector is 12 cm.](image)

![Fig. 7. Detector images of the incoherent irradiance with CPC as its antenna. (a) b=2 cm, θ₀=30°, h=10.4 cm; (b) b=2 cm, θ₀=30°, h=10.4 cm, radius of hemispheric lens R=2 cm; (c) b=1 cm, θ₀=30°, h=5.2 cm; (d) two CPCs in series, CPC₁: b=2 cm, θ₀=30°, h=10.4 cm; CPC₂: b=1 cm, θ₀=30°, h=5.2 cm. The distance from the light source to the upper surface of the CPC is 1.6 cm.](image)
Fig. 8. Pulse response curve.

Table 3. Measurement Results

<table>
<thead>
<tr>
<th>Receiving Angle (deg.)</th>
<th>$V_1$ (mV)</th>
<th>$V_2$ (mV)</th>
<th>Gain ($V_2/V_1$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>102</td>
<td>166</td>
<td>1.63</td>
</tr>
<tr>
<td>10</td>
<td>109</td>
<td>186</td>
<td>1.71</td>
</tr>
<tr>
<td>20</td>
<td>113</td>
<td>202</td>
<td>1.79</td>
</tr>
<tr>
<td>30</td>
<td>119</td>
<td>219</td>
<td>1.84</td>
</tr>
<tr>
<td>40</td>
<td>124</td>
<td>233</td>
<td>1.88</td>
</tr>
<tr>
<td>50</td>
<td>130</td>
<td>253</td>
<td>1.95</td>
</tr>
</tbody>
</table>

$V_1$ is the result without using antenna, $V_2$ is the result using CPC antenna.

In conclusion, we discuss the CPC used as a receiving antenna in atmosphere scattering optical communication. CPC’s structure is merely determined by $\theta_0$ and $b$, and light within the field of view would be absolutely reflected to the bottom aperture. CPC has the traits of large field of view and high gain. CPC employed as a receiving antenna in scattering optical communication can efficiently increase the corresponding range. In the next step, we will enhance the process level of CPC and do some experiments.

This work was supported by the National Natural Science Foundation of China under Grant No. 60607013.

References