MB-OFDM UWB over fiber system with direct detection

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We experimentally demonstrate the multiband orthogonal frequency-division multiplexing ultra-wideband (MB-OFDM UWB) over fiber system with direct detection. Different sub-carrier modulation formats (quadrature phase shift keying (QPSK) and 16 quadrature amplitude modulation (QAM)) are investigated in the MB-OFDM UWB over fiber system. The experimental results show that a 3.84 Gb/s 16 QAM-encoded MB-OFDM UWB signal can be successfully transmitted over 70 km standard single-mode fiber without chromatic dispersion compensation.

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Multiband orthogonal frequency-division multiplexing ultra-wideband (MB-OFDM UWB) over fiber system has paid more and more attention in the future broadband wireless communication owing to its capability to decrease the frequency selective fading caused by multipath effect[1-3]. Meanwhile, it can increase the area of coverage and provide high-speed data transmission[4-6]. Yee et al.[5] found that directly modulated laser-based MB-OFDM UWB signals can transmit over up to 5 km of standard single-mode fiber (SSMF). Moreover, MB-OFDM UWB signals based on external modulation can transmit up to 40 km of SSMF[6]. However, highly received optical power is required. As it is known, MB-OFDM UWB signal can share the spectrum with the existing radio communications systems. Hraimel et al.[7] investigated the performance of MB-OFDM UWBoF transmission system, considering the effect of in-band narrowband jammers such as WiMAX, MIMO WLAN, WLAN, and marine radar. But it does not take into account the influence of first three bands of MB-OFDM UWB signal. Omomukuyo et al.[8] experimentally demonstrated the MB-OFDM UWB system applying digital pre-distortion scheme to improve transmission performance of the system. However, only first sub-band is studied.

In this letter, we experimentally investigate the performance of MB-OFDM UWB signal transmission over fiber system. The first three sub-bands of MB-OFDM UWB signal transmission performance are evaluated by measuring the receiver sensitivity, error vector magnitude (EVM), and constellation diagram. The experimental results show that 3.84 Gb/s 16 quadrature amplitude modulation (QAM)-encoded MB-OFDM UWB signals can be successfully transmitted over 70 km SSMF without chromatic dispersion compensation.

The American Federal Communications Commission was the first to open radio spectra of 3.1–10.6 GHz with a spectrum width of 7.5 GHz for UWB use[9]. In the IEEE 802.15.3a standard, the spectrum width of MB-OFDM UWB signal is divided into 14 bands, and each band has a bandwidth of 528 MHz. The 14 channels are organized into five groups, as shown in Fig. 1. Each group has three channels from groups one to four and only two channels in group five. In fact, due to the constraint of current hardware, only the first three bands are investigated. Moreover, the center frequencies of the first three bands are $f_1 = 3.432 \text{ GHz}$, $f_2 = 3.960 \text{ GHz}$, and $f_3 = 4.488 \text{ GHz}$, respectively. To transmit three sub-bands of the MB-OFDM UWB signals simultaneously, the signal follows simple frequency-hopping sequences, such as $f_1$, $f_2$, and $f_3$. Figure 2 shows the three bands with time–frequency code (TFC2) in the time domain[9].

The architecture of the MB-OFDM UWB over fiber system is shown in Fig. 3. In the transmitter, the continuous light wave from the external cavity laser (ECL) is modulated by a Mach–Zehnder modulator (MZM). The pseudo-random binary sequences (PRBSs) are fed into an interleaver. Then, the output bits are mapped into quadrature phase shift keying (QPSK) or 16 QAM symbols. After inserting the pilots, the digital baseband OFDM symbol can be constructed by using inverse fast Fourier transform (IFFT). Therefore, the baseband OFDM symbol can be written as

$$S_{BB-OFDM}(t) = \sum_{k=-\frac{N_k}{2}}^{\frac{N_k}{2}} C_k \exp(\jmath 2\pi f_k t),$$

(1)

Fig. 1. Spectrum of MB-OFDM UWB signal band groups.
where $N_{ST}$ is the total number of sub-carrier, and the frequency of the $k$ sub-carrier is $f_k$. After adding the cyclic prefix (CP), digital-to-analog conversion (DAC), and intermediate frequency (IF) up-conversion with TFC, the IF MB-OFDM UWB signal is used as a radio frequency to the MZM. In addition, the IF MB-OFDM UWB signal can be expressed as

$$S_{\text{Ele-UWB}}(t) = \Re\left\{ \sum_{n=1}^{N_{ST}} \sum_{k=-N_{2}}^{N_{2}} C_k \exp(i2\pi f_k (t - n T_{\text{SYM}})) \right\},$$

(2)

where $f_k[q(n)]$, $N$, and $T_{\text{SYM}}$ are the carrier frequency functions of the MB-OFDM UWB signal, the number of OFDM symbols, and the symbol period, respectively. $\Re[\cdot]$ represents the real value of the electrical MB-OFDM UWB signal and $q(n)$ is a function that maps the $n$th OFDM symbol to the appropriate frequency with TFC.

Consequently, the MB-OFDM UWB signal is applied to the MZM to modulate a light wave with an optical carrier frequency $f_c$. The relationship between MZM driving voltage and optical field at MZM output is given by

$$S_{\text{Opt-UWB}}(t) = \sqrt{2P_{in}} \cos(2\pi f_c t + \phi_c(t)) \cdot \left[ \frac{\pi S_{\text{Ele-UWB}}(t) + V_{\text{bias}}}{V_x} \right],$$

(3)

where $V_{\text{bias}}$ denotes the direct current (DC) bias voltage, which is introduced to enable the MB-OFDM UWB demodulation using the direct detection and $V_x$ is the voltage required to induce a $\pi$ phase shift at the MZM.

At the receiver, the generated photocurrent $I(t)$ of the photo-detector (PD) can be expressed as

$$I(t) = \Re\left[ (S_{\text{Opt-UWB}}(t) + n(t)) * h(t) \right]^2
= \Re\left[ (S_{\text{Opt-UWB}}(t) * h(t))^2 \right] + \Re\left[ n(t) * h(t) \right]^2 + 2 \Re\left[ (S_{\text{Opt-UWB}}(t) * h(t)) * (n(t) * h(t)) \right].$$

(4)
received sensitivity of QPSK modulation is improved about 2 dB at the EVM of \(-17\) dB. Considering that the received optical powers are \(-13\) and \(-20\) dBm after 70 km SSMF transmission, the constellation diagrams of the two modulation formats are shown in Fig. 7. The constellation diagrams of QPSK and 16 QAM have serious deviation due to the chromatic dispersion of the fiber and optical amplifier noise. It is clearly seen that the performance of QPSK format is better than that of the 16 QAM at all of the received optical power. However, the bit rate of MB-OFDM UWB signal using QPSK format is only half of 16 QAM format.
Figure 8 shows the EVM of the received first three MB-OFDM UWB sub-bands. The higher order sub-band is impressionable by chromatic dispersion of the fiber at the received power of \(-13\) dBm. Comparing band 1 with band 3, the gain of both the QPSK and 16 QAM format is found to be 2 dB. With the decrease in the received power, the EVM is limited by electrical noise. The constellation diagrams of the two modulations are serious distortion at the received power of \(-20\) dBm. Therefore, the trend of EVM curves maybe to converge.

In conclusion, we experimentally investigate the performance of MB-OFDM UWB over fiber system. A 3.84 Gb/s 16 QAM-encoded MB-OFDM UWB signal can be successfully transmitted over 70 km SSMF without chromatic dispersion compensation. Compared with 16 QAM format, the received sensitivity of QPSK format is improved to about 2 dB at the EVM of \(-17\) dB. However, the higher order sub-band is impressionable by chromatic dispersion of the fiber.

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